Appendix 1. Model Archive Summary for Suspended-Sediment Concentration at U.S. Geological Survey Site 07182250, Cottonwood River near Plymouth, Kansas, during January 1, 2010, through April 22, 2015

This model archive summary summarizes the suspended-sediment concentration (SSC) model developed to compute hourly or daily SSC during January 1, 2010, through April 22, 2015. This model supersedes all prior models used during this period. The methods used follow U.S. Geological Survey (USGS) guidance as referenced in relevant Office of Surface Water/Office of Water Quality Technical Memoranda and USGS Techniques and Methods, book 3, chapter C4, and the policy and guidance for approval of surrogate regression models for computation of time series SSCs and loads (Rasmussen and others, 2009; U.S. Geological Survey, 2016).

Site and Model Information

Site number: 07182250

Site name: Cottonwood River near Plymouth, Kansas

Location: Lat 38°23'51", long 96°21'21" referenced to North American Datum of 1927, in NE 1/4 NE 1/4 SE 1/4 sec.13, T.19 S., R.9 E., Chase County, Kans., hydrologic unit 11070203, on right bank at upstream side of county highway bridge, 0.8 mile (mi) downstream from Buckeye Creek, 1.5 mi. southwest of Plymouth, and at mile 39.2.

Equipment: A YSI 6600 water-quality monitor equipped with sensors for water temperature, specific conductance, and turbidity (YSI model 6136 turbidity sensor). The YSI 6600 water-quality monitor was in operation during February 22, 2007, through May 23, 2009.

Date model was developed: January 16, 2020

Model calibration data period: March 26, 2007, through May 14, 2009

Model Data

All data were collected using USGS protocols (Wagner and others, 2006; Sauer and Turnipseed, 2010; Turnipseed and Sauer, 2010; U.S. Geological Survey, variously dated) and are stored in the National Water Information System (NWIS) database (https://doi.org/10.5066/F7P55KJN; U.S. Geological Survey, 2020). Explanatory variables were evaluated individually and in combination. Potential explanatory variables included streamflow, water temperature, specific conductance, and turbidity. Seasonal components were also evaluated as explanatory variables.

The regression model is based on 22 concurrent measurements of discretely collected SSC samples and continuously measured turbidity during March 26, 2007, through May 14, 2009. Discrete samples were collected over a range of streamflows and turbidity conditions. No samples had concentrations below laboratory detection limits. Identification of potential outliers included any values that exceeded the Cook's D test (Cook, 1977) and any point for which the studentized residual was greater than 3 or less than –3. None of the samples in this dataset were deemed outliers or removed from the model calibration dataset.

Suspended-Sediment Sampling Details

Discrete samples were collected from the downstream side of the bridge or instream within 400 feet of the bridge using equal-width-increment, multiple vertical, single vertical, or grab-dip methods following U.S. Geological Survey (2006) and Rasmussen and others (2014). Discrete samples were collected on a semifixed to event-based schedule ranging from 2 to 15 samples per year with a Federal Interagency Sediment Project U.S. DH–48, DH–59, DH–75P, or a D–95 with a Teflon bottle, cap, and nozzle depth-integrating sampler depending on sample location. Samples were analyzed for SSC, loss on ignition, and occasionally five-point grain size by the USGS Sediment Laboratory in Iowa City, Iowa.

Continuous Data

Turbidity was measured using a YSI model 6136 sensor installed during February 22, 2007, to May 23, 2009 (U.S. Geological Survey, 2018). Concomitant turbidity values were time interpolated. If continuous data were not available (2 or more hours of specific conductance values bracketing the sample collected time were missing) because of fouling, changes in equipment, or unsuitable site conditions, then the field monitor turbidity value measured during sampling was substituted. If neither concomitant continuous data nor field monitor data were available, the sample was not included in the dataset. The range of continuous turbidity data of the YSI model 6136 sensor (in formazin nephelometric units) was as follows: maximum 1,230; minimum 1.10; mean 76.2; median 27.0.

Model Development

Ordinary least squares regression analysis was done using R programming language (R Core Team, 2019) to relate discretely collected SSC to turbidity and other continuously measured data. The distribution of residuals was examined for normality, and plots of residuals (the difference between the measured and model calculated values) compared to model calculated SSC were examined for homoscedasticity (departures from zero did not change substantially over the range of model calculated values).

Turbidity was selected as the best predictor of logarithm base 10 (\log_{10}) (SSC) based on residual plots, relatively high coefficient of determination (R^2), and relatively low model standard percentage error (MSPE).

Model Summary

Summary of final SSC regression analysis at site 07182250: SSC-based model:

$$Log_{10}(SSC) = 0.931 \times Log_{10}(Turb6136) + 0.547$$

where

SSC = suspended-sediment concentration, in milligrams per liter, and Turb6136 = turbidity, YSI model 6136, in formazin nephelometric units.

The use of turbidity as an explanatory variable is appropriate physically and statistically. Turbidity makes sense physically because suspended sediment is composed of particles that scatter light in water. The relation between turbidity and SSC can vary given varying concentrations of organic suspended particles that increase turbidity but are not included in the SSC analysis.

The log-transformed model may be retransformed to the original units to calculate SSC directly. A bias is introduced in the calculated constituent during retransformation and may be corrected using the Duan's bias correction factor (BCF; Duan, 1983). The calculated BCF is 1.03 for this model, and the formula for the retransformed model accounting for BCF is as follows:

$$SSC = 3.63 \times Turb6136^{0.931}$$

Suspended-Sediment Concentration Record

The SSC record that is being used in this regression model is stored at the National Real-Time Water Quality (NRTWQ) website (https://nrtwq.usgs.gov/ks).

Previously Published Model

$$\log_{10}(SSC) = 1.02 \times \log_{10}(Turb) + 0.30$$

Model author: Foster (2014)

Model data period: June 17, 2009, through September 27, 2012

Model Statistics, Data, and Plots

Model

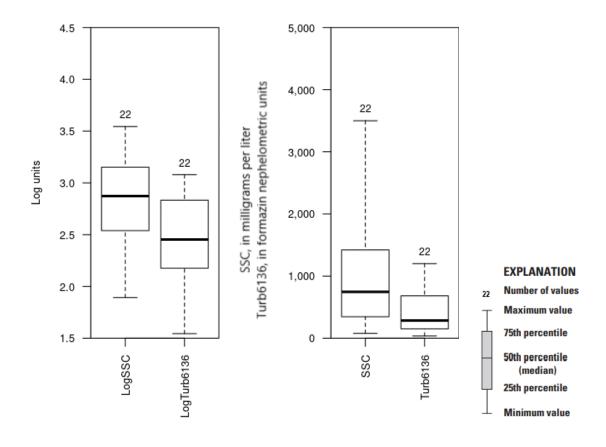
$$Log(SSC) = +0.931 * Log(Turb6136) + 0.547$$

Variable Summary Statistics

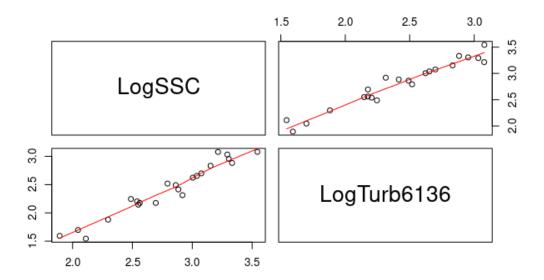
	LogSSC	SSC	LogTurb6136	Turb6136
Minimum	1.89	78	1.54	35
1st Quartile	2.54	346	2.18	150

Median	2.87 746	2.45	285
Mean	2.80 968	2.42	421
3d Quartile	3.15 1420	2.83	681
Maximum	3.54 3500	3.08	1200

Box Plots



Exploratory Plots



Basic Model Statistics

Number of Observations	22
Standard error (RMSE)	0.105
Average Model standard percentage error (MSPE)	24.5
Coefficient of determination (R2)	0.948
Adjusted Coefficient of Determination (Adj. R ²)	0.945
Bias Correction Factor (BCF)	1.03

Explanatory Variables

	Coefficients	Standard Error	t value	Pr(> t)
(Intercept)	0.547	0.1200	4.54	2.00e-04
LogTurb6136	0.931	0.0489	19.00	2.75e-14

Correlation Matrix

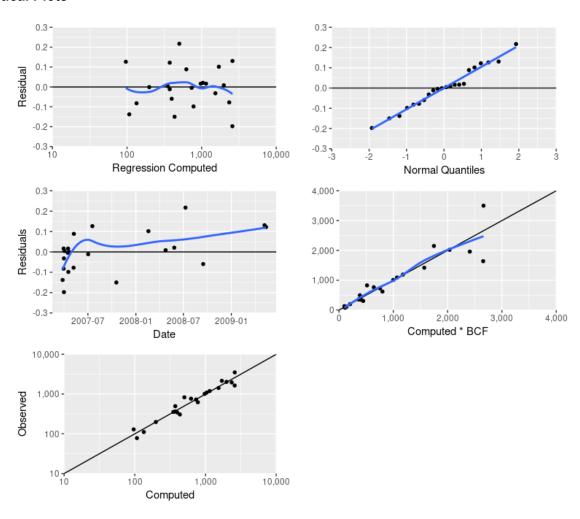
	Intercept E	E.vars
Intercept	ept 1.000 -	-0.982
E.vars	-0.982	1.000

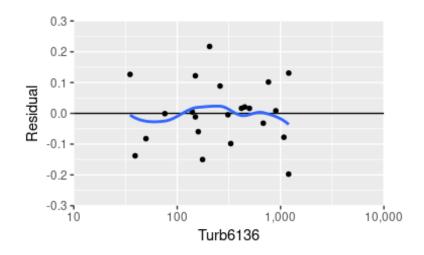
Outlier Test Criteria

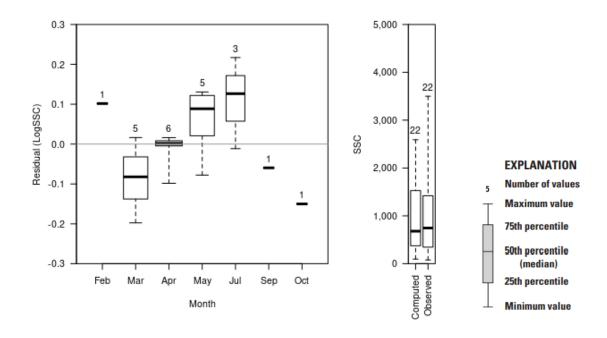
Flagged Observations

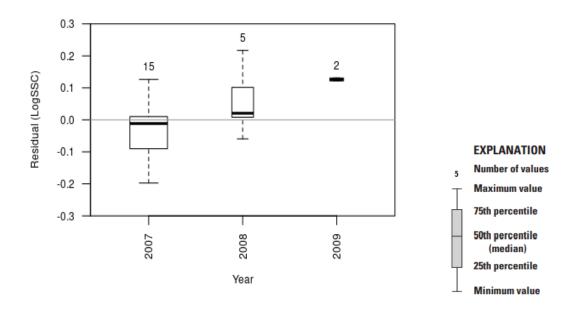
	LogSSC	Estimate	Residual	Standard Residual	Studentized Residual	Leverage	Cook's D DFFI	TS
3/26/2007 12:05	1.89	2.03	-0.138	-1.46	-1.50	0.193	0.253 -0.73	33
3/31/2007 8:25	3.21	3.41	-0.198	-2.02	-2.21	0.139	0.328 -0.88	85
7/18/2007 11:15	2.11	1.98	0.126	1.35	1.38	0.211	0.243 0.73	13

Statistical Plots

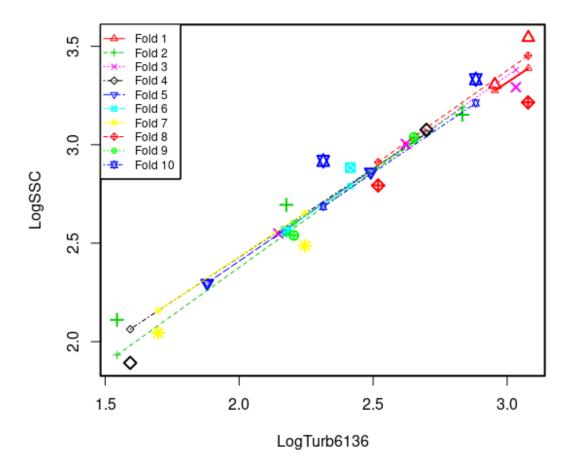








Cross Validation



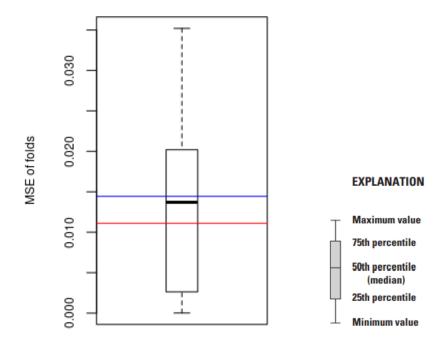
```
Minimum mean squared error (MSE) of folds: 1.26e-05

Mean MSE of folds: 1.44e-02

Median MSE of folds: 1.37e-02

Maximum MSE of folds: 3.52e-02

(Mean MSE of folds) / (Model MSE): 1.30e+00
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Red line - Model MSE

Blue line - Mean MSE of folds

Model-Calibration Dataset

	Date	LogSSC	LogTurb6136	SSC	Turb6136	Computed	Computed	Residual	Normal	Censored
0						LogSSC	SSC		Quantiles	Values
1	2007-03-26	1.89	1.59	78	39.2	2.03	110	-0.138	-1.19	
2	2007-03-30	2.05	1.7	111	49.9	2.13	138	-0.0822	-0.816	
3	2007-03-30	3	2.62	1010	419	2.99	999	0.0164	0.406	
4	2007-03-31	3.21	3.08	1640	1200	3.41	2650	-0.198	-1.93	
5	2007-03-31	3.15	2.83	1420	681	3.18	1570	-0.032	-0.406	
6	2007-04-02	2.55	2.15	354	140	2.54	360	0.00432	0.0565	
7	2007-04-15	2.86	2.49	727	310	2.87	755	-0.00457	-0.17	
8	2007-04-16	3.08	2.7	1190	500	3.06	1180	0.0162	0.286	
9	2007-04-17	2.79	2.52	621	330	2.89	800	-0.0983	-0.986	
10	2007-04-20	2.3	1.88	198	76	2.3	204	-0.00101	-0.0565	
11	2007-05-07	3.29	3.03	1960	1080	3.37	2410	-0.0778	-0.667	
12	2007-05-08	2.88	2.41	765	260	2.79	641	0.0887	0.667	
13	2007-07-02	2.56	2.18	364	150	2.57	384	-0.0115	-0.286	

1	4 2007-07-18	2.11	1.54	129	35	1.98	99	0.126	1.19	
1	5 2007-10-18	2.49	2.25	307	176	2.64	446	-0.15	-1.46	
1	6 2008-02-18	3.33	2.88	2150	764	3.23	1750	0.102	0.816	
1	7 2008-04-24	3.31	2.95	2020	900	3.3	2040	0.0083	0.17	
1	8 2008-05-27	3.04	2.65	1090	450	3.02	1070	0.0206	0.532	
19	9 2008-07-09	2.92	2.31	828	206	2.7	516	0.217	1.93	
2	0 2008-09-15	2.54	2.2	346	160	2.6	408	-0.0596	-0.532	
2	1 2009-05-08	3.54	3.08	3500	1200	3.41	2660	0.131	1.46	
2	2 2009-05-14	2.69	2.18	495	150	2.57	384	0.122	0.986	

Definitions

Adj R²: Adjusted coefficient of determination

BCF: Bias correction factor

DFFITS: Studentized difference in fits

Log: logarithm base 10

MSE: Mean squared error

MSPE: Model standard percentage error

R²: Coefficient of determination

RMSE: Root mean square error

SSC: Suspended-sediment concentration, in milligrams per liter (80154)

Turb6136: Turbidity, in formazin nephelometric units (63680)

Any use of trade, firm, or product names is for descriptive purposes only and does not imply endorsement by the U.S. Government.

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